

Rolling Ball Viscometry for Molten Salts: Ensuring Measurement Accuracy, Quantifying Uncertainty

Workshop on Measurement and Analysis of Thermochemical & Thermophysical Properties of Molten Salts

<u>July 17th, 2024</u>

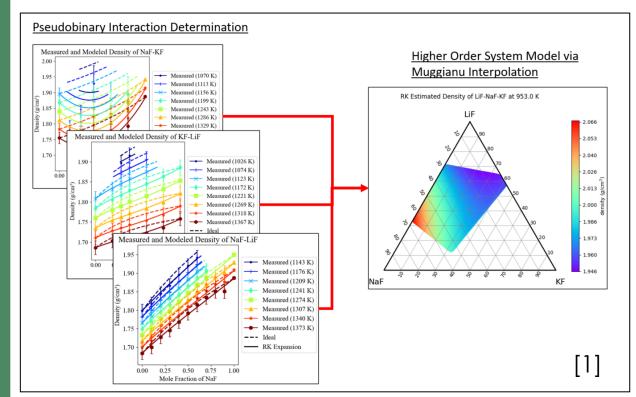
Anthony Birri, Nicholas Termini, Ryan Chesser, Kevin Garland, Craig Gray, Ethan Wilgocki, N. Dianne Bull Ezell

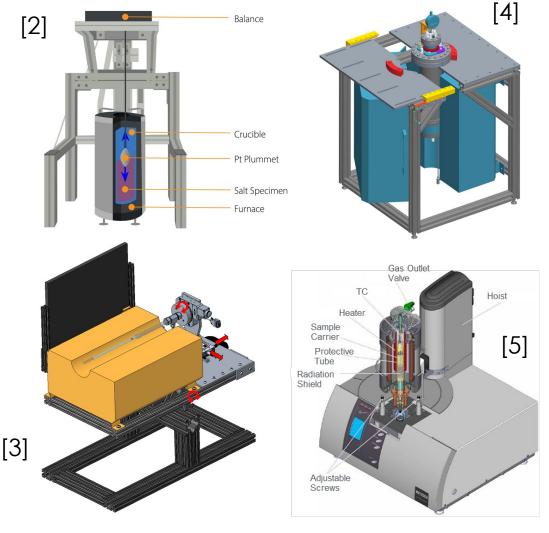
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Overview of Thermophysical Characterization Efforts at ORNL

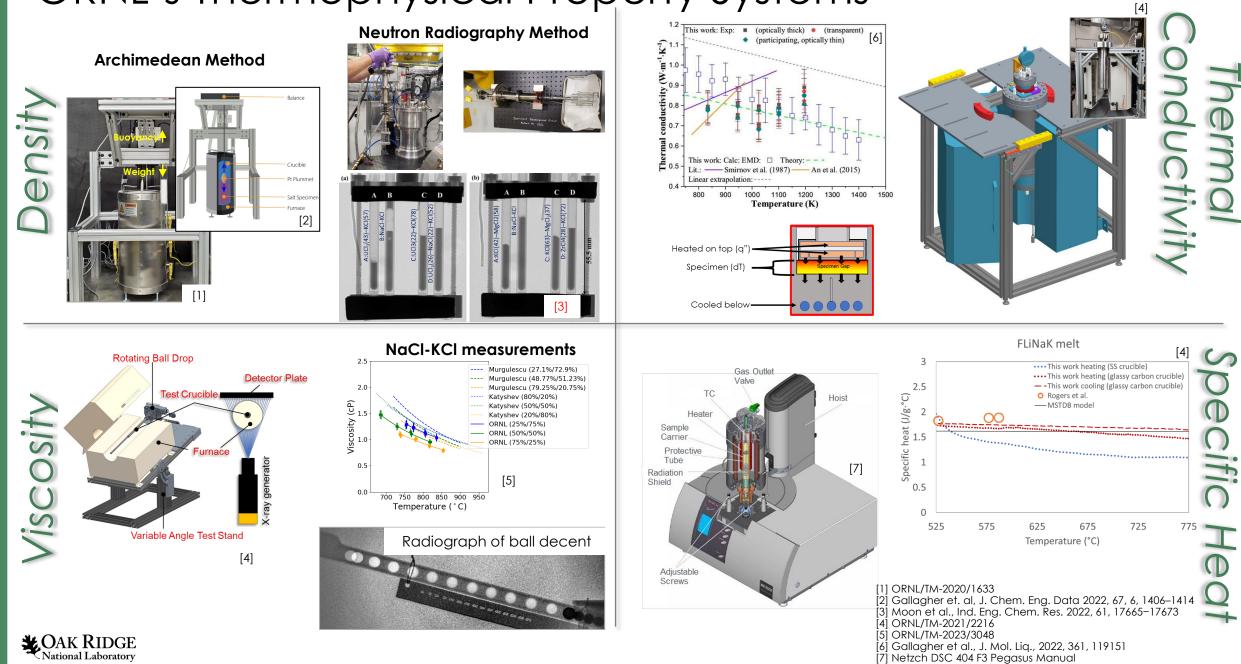
- 1. Experimental Measurements
- 2. Database Development
- 3. Predictive Modeling





ORNL/TM-2023/2955
 Gallagher et. al, J. Chem. Eng. Data 2022, 67, 6, 1406–1414
 Birri et al. (2023). TSEP, 44, 102029.
 ORNL/TM-2020/1633
 Netzch DSC 404 F3 Pegasus Manual

ORNL's Thermophysical Property Systems



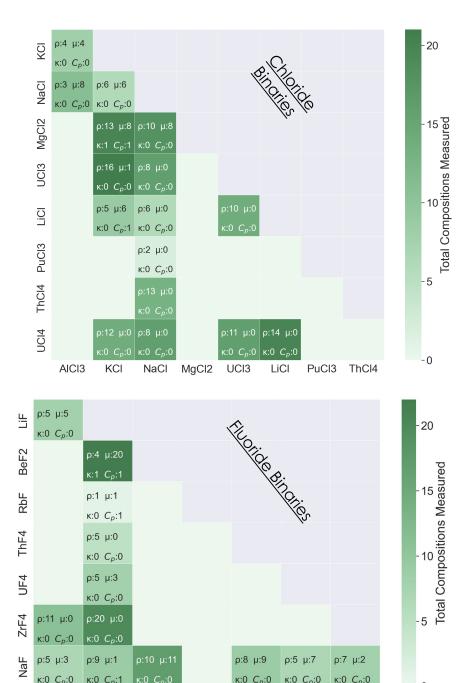
Gaps in Viscosity Characterization

- Generally very few studies on actinidebearing melt viscosity
 - For chlorides, limited to the data generated from a single group in Russia in the 70s through the 90s [1]
 - For fluorides, limited to a few studies by Blanke in the 50s [2, 3]
 - No duplicate studies to compare against
- No understanding of UF3-UF4, BeF2-UF3, BeF2-UF4, UF4-ZrF4, MgCl2-UCl3
 - However some higher order systems with these subsystems have been studied
- Nothing on PuCl3 bearing melts

坐 Oak Ridge

 Katyshev, Sergey Filippovich. Properties of molten mixtures of alkali metal halides, zirconium, hafnium and uranium. Ural State Technical University, 2001.
 Blanke, B. C et al. Viscosity of Fused Mixtures of Sodium Fluoride, Beryllium Fluoride, and Uranium Fluoride. Mound Laboratory. 1958b.

[3] Blanke, B.C et al. Density and Viscosity of Fused Mixtures of Lithium, Beryllium, and Uranium Fluorides. Mound Laboratory. 1959



LiF

BeF2

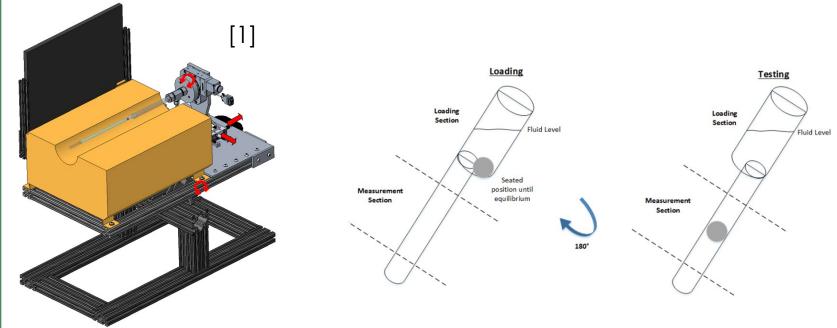
RbF

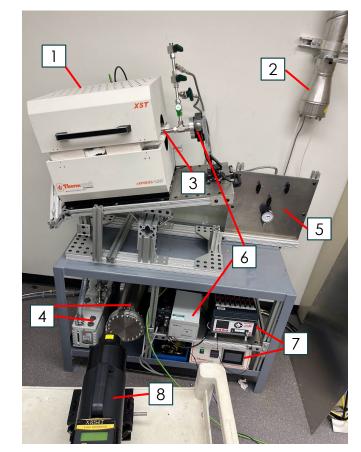
ZrF4

KF

Overview of System

- Based on Rolling Ball Technique
 - Terminal velocity of ball corresponds with viscosity of fluids
 - Correlation determined based on calibration with NIST standard oils
- Oxygen filter integrated (~ppb levels)
- Designated CA zone and ventilation to enable actinide salt measurements
- New x-ray system which requires minimal image processing
 - Used for stainless steel crucibles
 - For fluoride and actinide bearing salts which can't be contained in fused quartz





- Furnace
 Ventilation
 Crucible
- 4. Backfill/
 - pressure maintenance
 - system

- Gas control
 Rotation control
 - Rotation control
- 7. Heating/temper ature control
- 8. X-ray system (detector behind furnace

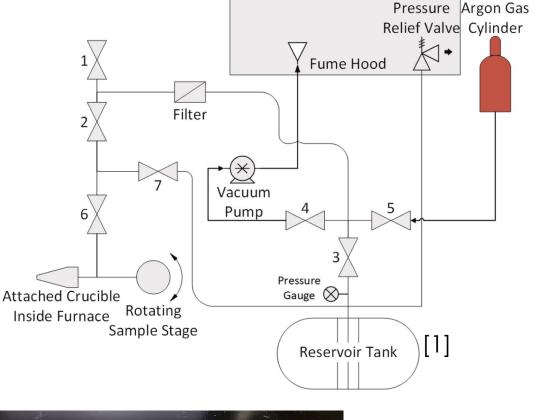
Birri et al. (2023). TSEP, 44, 102029.
 ORNL/TM-2020/1633

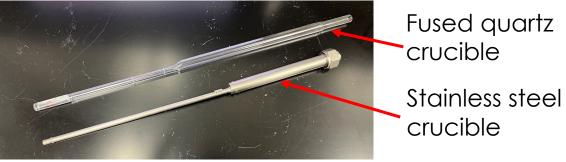
How the Measurement is Conducted

- 1. The crucible is calibrated over a range of Re and d/D ratios with NIST standard oils
- 2. The crucible is loaded with purified salt in a glovebox and valved off
- 3. The entire system is backfilled with Ar
- 4. The crucible is attached to the system and control volumes are combined
- 5. The system is brought to desired temperature

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6. Balls enter through load lock, terminal velocity is measured. Triplicate measurements at each temperature.





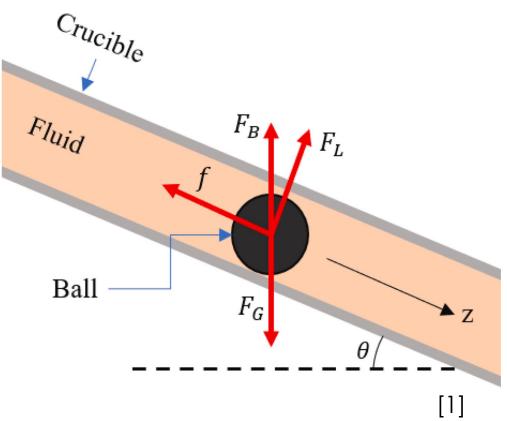


General Working Equation

• After balancing of forces [1], one arrives at:

$$\mu = \frac{K(\rho_b - \rho_f)tsin(\theta)}{L}$$

- *K* is a calibration factor, dependent on wall effects and flow conditions
- ho_b is the density of the ball
- ρ_f is the density of the fluid
- t is the time to roll a specified distance
- θ is the angle of inclination
- *L* is the specified rolling distance



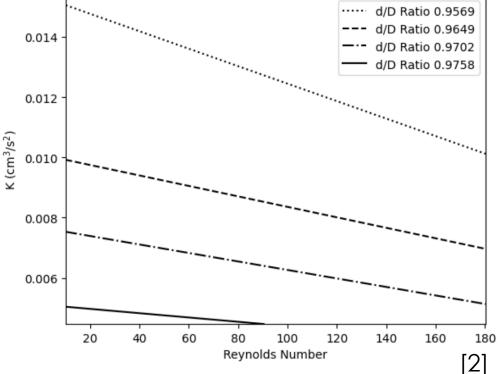
- F_B is the buoyancy force
- f is the opposing viscous force, involves K and μ
- F_L is the lift force
- F_{G} is the gravitational force



Determination of K

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- There are several studies to describe K mathematically, but we have not found one which seems accurate based on oil experiments
 - This is likely a consequence of the difficulty to characterize Re >> 1 (our situation with low viscosity salts)
- Therefore, we must develop a calibration curve for $K\left(Re, \frac{d}{D}\right)$
 - From thermal expansion mismatch of ball and crucible, $\frac{d}{D}$ changes
 - If you know d(T) and D(T), you can get K(Re,T)



Example Calibration Curves

- Note that this linear functionality is ONLY observed for laminar regime
- For lower Re (Stokes flow, Re <1) and higher Re (formation of turbulent wake, Re>>100) things change

[2] ORNL/TM-2023/3048

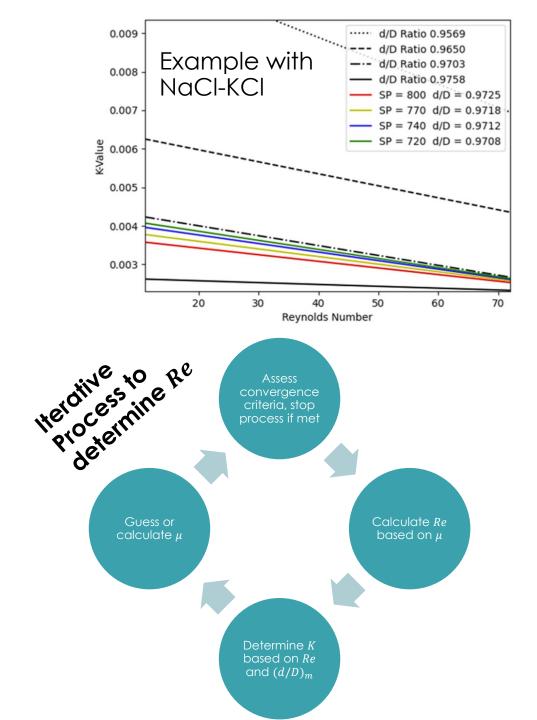
How we determine K for some arbitrary salt measurement

- 1. Measure a range of oils at different angles and ball sizes to measure K for a range of Re and d/D ratios
 - This yields a series of curves (with index *i*) defined by $K(d/D = (d/D) \cdot P_{i} = a_{i} + b_{i} + P_{i}$

 $K(d/D = (d/D)_i, Re) = a_i + b_i * Re$

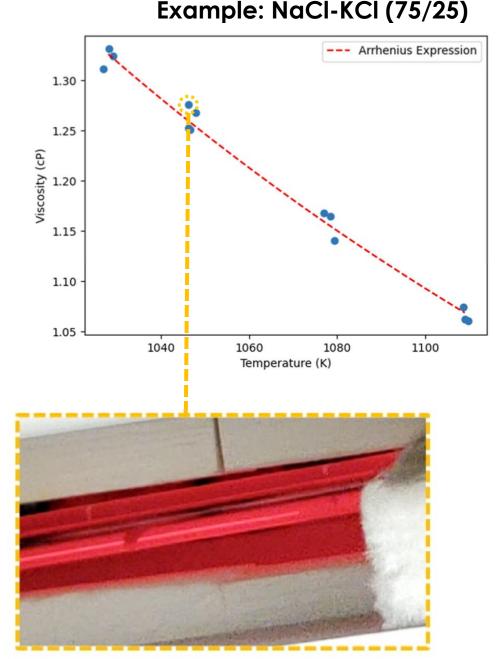
- 2. Determine the measured salt $(d/D)_{m}$, and determine calibration curve for measurement
 - $K(d/D = (d/D)_m, Re) = a_m + b_m * Re$
 - a_m and b_m determined through interpolation
- 3. Iteratively determine *Re* based on calibration curve

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What the Data Ends up Looking Like

- After going through the complicated process of calibrating the crucible and determining K, we expect an Arrhenius relation with temperature
 - i.e. $\mu = Ae^{B/RT}$
 - This has generally been used for molten salts, assumes Newtonian fluid
- Typically 4 setpoints, 3+ datapoints at each setpoint
 - Triplicate measurements yield an understanding of measurement accuracy
- All calculations are automated in Python, we just need to supply angles, temperatures, and terminal velocities
 - True for calibration curve generation and salt measurement





Sources of Uncertainty

- Temperature
 - Both from thermocouples and difference in thermocouple/salt temperatures
- Salt density

SOAK RIDGE

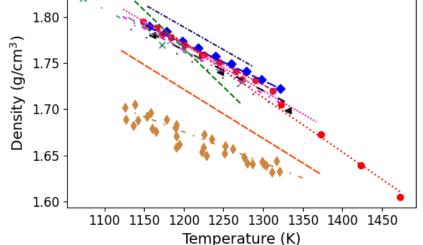
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- Some salts are more well characterized than bothers
- Thermal expansion of ball and crucible
 - Glass thermal expansion is relatively uncertain
- Angle, distance, and time measurements subject to instrument precision limits

[1] J. Oishi and T. Kimura. Thermal expansion of fused quartz. Metrologia, 5(2):50, 1969.

Example of LiF salt density spread





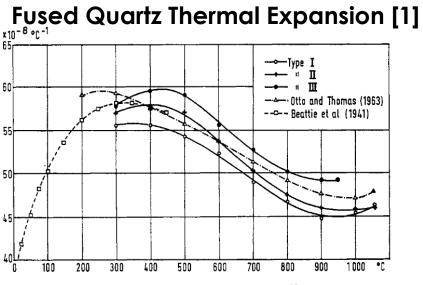


Fig. 7. Comparison of mean expansion coefficient $\overline{\alpha}_0^t$

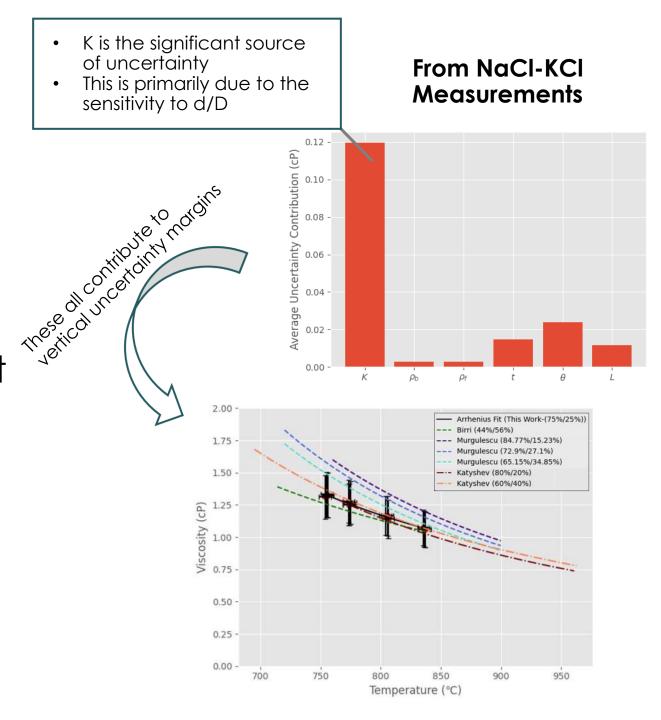
Uncertainty Propagation

• Use Gaussian error formalism for μ

$$\sigma_{\mu}^{2} = \left(\frac{\partial \mu}{\partial K}\sigma_{K}\right)^{2} + \left(\frac{\partial \mu}{\partial \rho_{b}}\rho_{b}\right)^{2} + \dots$$

- For *T*, simply calculate $\mu(T + \sigma_T)$ and $\mu(T \sigma_T)$ to get error bar on temperature axis
- Euclidian distance gives total uncertainty:

-
$$\sigma_{tot}^2 = \sigma_{\mu}^2 + \sigma_T^2$$





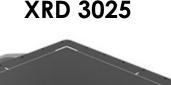
X-ray Compatibility

- Fluoride salts and actinide salts need to be contained in steel crucibles
 - Fluorides etch glass
 - We need to eliminate risk of dispersing actinides
- We have an XRS4T X-ray source by Golden Engineering
 - 370 kV
 - Up to 9 pulses per second
- XRD 3025 Detector Plate by Varex Imaging
 - 3008 x 2512 pixel matrix (100 μ m pixel pitch)
- Alkali halides have good x-ray transparency, actinides have higher attenuation leading to darker images
- These devices allow for rapid enough images collection for terminal velocity measurements



XRS4T

https://www.goldenengineering.com/products/xrs4/





https://www.x-innovations.co.uk/wp-content/uploads/2019/05/XRD-3025.pdf



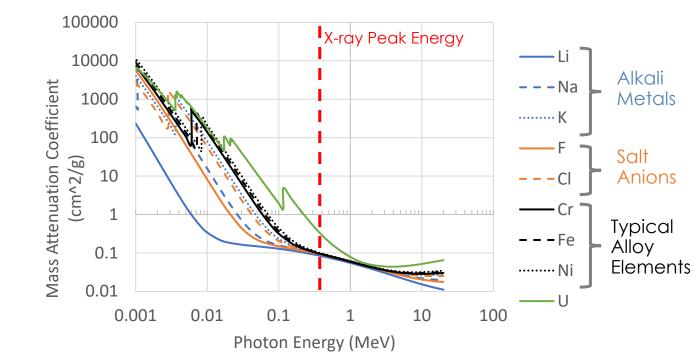
X-ray Advantages and Disadvantages

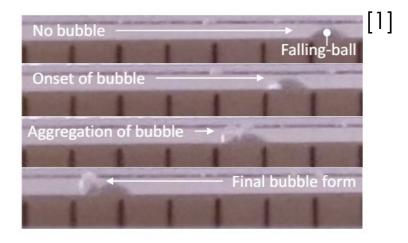
Advantages

- Allows for measurement of a wider array of salts
- Easier path for image processing automation with built in software
- No real risk of crucible breaking
- Thermal expansion matching→ BIG uncertainty reduction

• Disadvantages

- Crucibles are challenging to manufacture and time consuming
- May be harder to see bubbles (salt dependent)
- Some salts may make seeing the ball a challenge

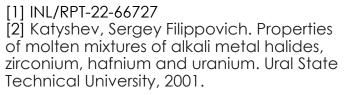


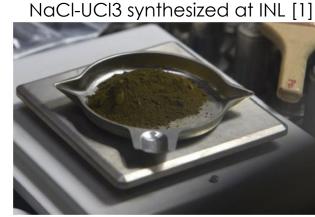


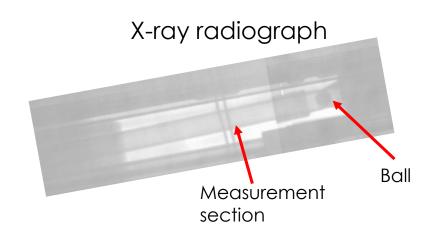
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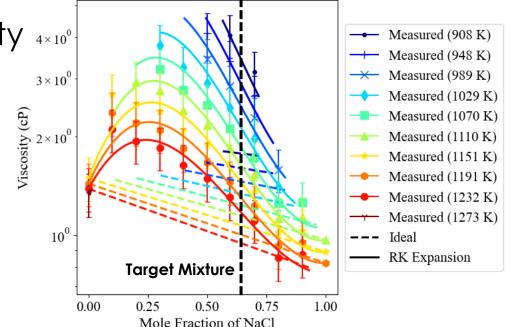
Plans to Measure NaCI-UCI3

- Planning to conduct actinide salt measurements in 2024
 - These will make use of stainless steel crucibles and x-ray radiography
- The target mixture to measure first is NaCI-UCI3
 - Synthesized at INL [1] (POC: Bill Phillips)
 - Already measured thermal conductivity
- We can compare our measurements to Russian literature on actinide chloride viscosity 4×10° [2]







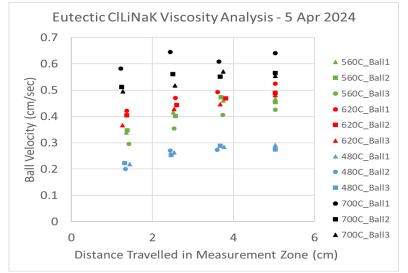


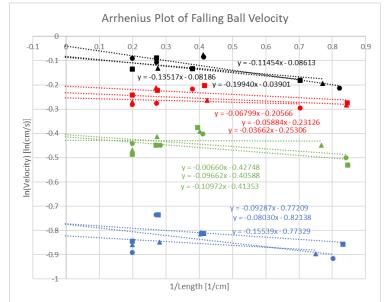
Technical University, 2001. **CAK RIDGE**

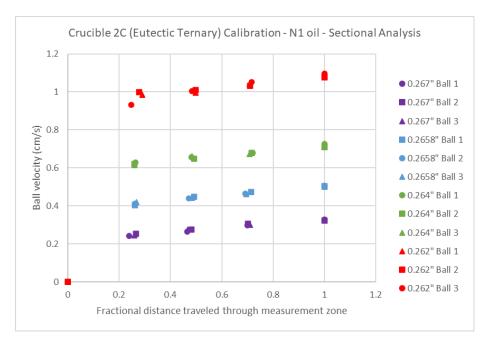
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Terminal Velocity: Additional Source of Uncertainty?

- We are realizing that the ball is still speeding up in test section after more careful analysis
 - Assumptions about rapidly meeting terminal velocity may not be right
- Currently assessing if calibration data automatically captures this
- If not, we can exponentially extrapolate to get terminal velocity
- A longer distance before the measurement section could also solve this problem



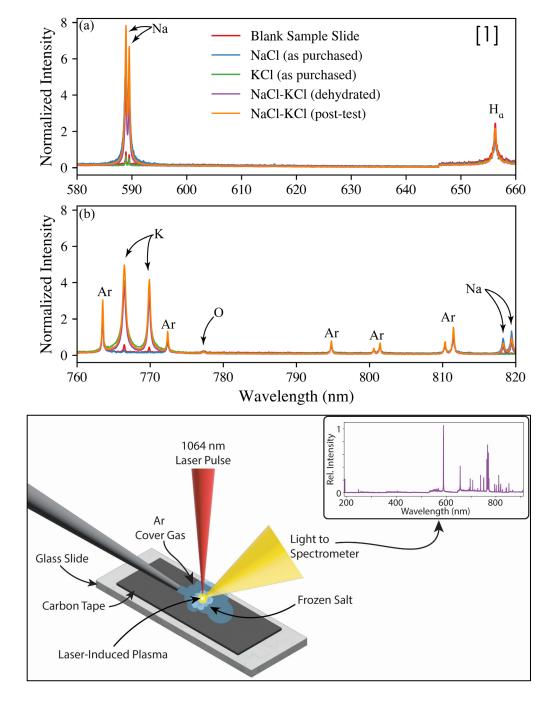






Ensuring Salt Purity

- Alkali Halides are always purchased with minimal possible trace metal basis (Sigma Aldrich)
- Lab synthesized salts assessed with ICP-OES, ICP-MS, or XRD
 - We work with synthesizers for analysis
 - Much credit to Bill Phillips (INL), Zach Huber and Bruce McNamara (PNNL), and Amanda Leong (VT)
- Pre and post test LIBS to check for O and H impurities (Hunter Andrews, ORNL)



Summary

- Rolling ball viscometry is one method which can be used for measuring molten salt viscosity
- The working equation allows for full propagation of uncertainty
- Glass crucibles can be used which, thus far, have allowed for more rapid, inexpensive measurements
- Stainless steel crucibles can be used for salts which require this material, and they enable uncertainty reduction
- We have measured several alkali halide mixtures and a measurement of NaCl-UCl3 is upcoming

This work is directly funded by the Molten Salt Reactor Campaign and the Nuclear Energy Advanced Modeling and Simulation Program under the Department of Energy, Office of Nuclear Energy.

The authors would like to acknowledge Joanna McFarlane and Kevin Robb for their molten salt expertise which has better informed decisions made in this work, Hunter Andrews for his collaboration on LIBS measurements of salt samples, and Callie Goetz on automation of the crucible rotation system.